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Optical partitioning for multicarrier generation in subcarrier multiplexed networks

Particionado óptico para la generación multiportadora en redes multiplexadas en subportadora

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Abstract

Objective– To evaluate the multicarrier generation technique based on spectral segmentation for the transport of optical subcarrier multiplexing signals.

Methodology- The proposal is evaluated through experimental validation and modeling based on simulation of the generation of optical carriers using a broadband source in combination with an optical filter configured with different pass bands and transmission at different distances.

Results– The experimental evaluation measured the Error Vector Magnitude (EVM) for 1nm, 3nm, 6nm and 8nm optical slices that transport QPSK and 16QAM modulation formats at 1 GHz and 3 GHz subcarriers over a fiber link of 10 km. For the case of 1nm pass band and QPSK modulation, an EVM of 29.6458% was found while an EVM of 40.4685% for the service transported in 16QAM was measured. The simulation model showed that a bit error rate of 1x10⁻¹² is achieved for spectral partition sizes of 100MHz on 5GH, 30GHz and 60GHz subcarriers.

Conclusions- The experimental results showed that the measured EVM did not show significant difference regarding the subcarrier frequency for a QPSK service. However, the 16QAM modulation is recommended only when the subcarrier frequency is 1GHz or below for a correct equalization of the received signal. Simulation modeling evaluated the approach at higher subcarrier frequencies and longer distances, results found show that a 60GHz subcarrier over a fiber link of 40km is feasible for a slice size of 100MHz.

Resumen

Objetivo– Evaluar la técnica de generación multiportadora basada en segmentado espectral para el transporte de señales de señales multiplexadas en subportadora óptica.

Metodología- La propuesta se evalúa mediante validación experimental y modelamiento basado en simulación de la generación de portadoras ópticas utilizando una fuente de banda ancha en combinación con un filtro óptico configurado con diferentes bandas de paso y transmisión a diferentes distancias.

Resultados- La evaluación experimental midió la magnitud del vector de error para particiones espectrales de 1nm, 3nm, 6nm y 8nm que transportan formatos de modulación QPSK y 16QAM en subportadoras de 1 GHz y 3 GHz a través de un enlace de fibra de 10 km. Para una banda de paso de 1nm y modulación QPSK, se encontró un EVM de 29.6458% mientras que un EVM de 40.4685% fue medido para el servicio transportado en 16QAM. El modelo de simulación mostró que una tasa de error de bit de 1x10⁻¹² se logra para tamaños de particiones espectrales de 100MHz en subportadoras de 5GH, 30GHz y 60GHz. **Conclusiones**– Los resultados experimentales mostraron que el EVM medido no mostró una diferencia significativa con respecto a la frecuencia de la subportadora para un servicio QPSK. Sin embargo, la modulación 16QAM se recomienda solo cuando la frecuencia de la subportadora es 1 GHz o inferior para una ecualización correcta de la señal recibida. El modelo de simulación evaluó la propuesta en frecuencias subportadoras más altas y distancias más largas. Los resultados encontrados muestran que una subportadora de 60 GHz sobre un enlace de fibra de 40 km es posible cuando el tamaño de la partición óptica es de 100MHz.

Keywords- Spectral partitioning, subcarrier multiplexing, wavelength division multiplexing, Radio over Fiber, Optical access networks, Broadband optical sources

Palabras clave-Particionado espectral; Multiplexación de subportadora; Multiplexación por división de longitud de onda; Radio sobre fibra; Redes de acceso óptico; Fuentes de banda ancha

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I. INTRODUCTION

The advent of future 5G networks is putting into evidence the need for a convergence of wireless and optical networks in order to ease the network evolution towards the transport of high-capacity mobile devices and data-intensive applications [1]. This convergent scenario envisages that both mobile and fixed services will be transported and distributed using the same physical platform. In this context, the use of Radio over Fiber (RoF) techniques based on Subcarrier Multiplexing (SCM) provides a new level of multiplexing over each optical channel that facilitates the transport of mobile services directly on its original radio frequency signal. This fact enables a WDM-SCM hybrid-multiplexing system, in which there is an independent information channel for each one of the subcarriers that make up each one of the WDM optical channels. The advantage of this combined multiplexing scheme is that it enables each carrier to be routed to a specific radio front-end based on the wavelength value. Thus, it is envisaged a wide range of new strategies to provide transport services for small and dense cells to cost-effectively support the continuous cell densification [2]. One of such strategies deals with the reduction of the optoelectronic devices used in the transmitting side of an optical network. In this context, multicarrier generation techniques have attracted attention in order to provide solutions for the growing deployment of fixed and mobile broadband networks.

Related work has dealt with multicarrier generation based on optical frequency comb shaping techniques. Recently, an approach using three modulators in cascade and a laser source that is connected with one amplitude modulator and two Mach-Zehnder Modulators (MZMs) in cascade is described [3]. In this approach, a multi-carrier optical generator on the side of the OLT that supports numerous users, reduce the costs of the Optical Line Terminal (OLT) of the conventional Wavelength Division Multiplexed Passive Optical Network system (WDM-PON). Also, an approach that generates optical carriers provided by an optical frequency comb with externally injected gain switching is presented [4]. In such proposal each optical channel transmitted an orthogonal subcarrier multiplexing (SCM) signal of 21.6 Gb/s at 30 GHz which was modulated and demodulated in the electrical domain. Another channelization scheme for a wideband radio-frequency (RF) signal based on an Optical Frequency Comb (OFC) is presented where a comb filter and an optical demux is proposed and demonstrated [6]. In this approach, the input broadband Radio Frequency (RF) signal is multicast by a 39GHz-spaced OFC and sliced by a Fabry–Pérot filter (FPF). Also, an approach for fast wireless information transmission using spectrumsliced super-continuum along the THz frequency range is described [7] and a demonstration of a spectrum-sliced wavelength division multiplexed passive optical network with the channel spacing of 25 GHz is presented [8].

In this work, we propose an optical architecture for the multicarrier generation in subcarrier multiplexing networks. The approach is assessed in a testbed and subsequently a simulation model allows evaluating its performance at different subcarrier frequencies, distances and pass band values. The underlying contribution of this work lies in the simplified way of generating multiple optical channels based on the spectral partitioning of a broadband optical source through a wideband optical filter. Unlike the related proposals described previously, this approach enables the generation and transport of optical carriers to feed the SCM network using wider pass bands than those used and demonstrated in the state of the art. We believe that this unique feature leads to a cost-effective multicarrier generation system for subcarrier multiplexed transport in network segments covering the required distances of future small cells and high density cells scenarios expected in future 5G networks.

This paper is organized as follows, section 2 describes the proposed architecture and the implementation details of the approach, section 3 presents and discusses the experimental and modeling results and section 4 summarizes the paper.

II. MATERIALS AND METHODS

Fig. 1 shows the layout of a subcarrier-multiplexed network in which our approach can be included in order to provide the optical carriers. Overall, the system consists of a broadband source that feeds the demux filter responsible for partitioning the optical spectrum emitted by the broadband source. After carrier generation, a multiplexed comb is sent to the access segment through the optical circulator (a), which directs the unmodulated carrier to the optical modulator in each one of the base stations of the access network to conform the uplink signal in this segment. Once the RoF signal has been obtained, the optical circulator (b) enables the uplink and directs the signal towards the metro network. Subsequently, a 1x2 optical splitter is responsible for distributing the RoF signal equally to the Optical Add-Drop Multiplexer (OADM). The OADM consists of optical switches and an arrangement of Arrayed Waveguide Gratings (AWG), which are in charge of defining the inputs and outputs of the system.

A. Implementation details

The experimental setup shown in Fig. 2 includes a Broadband Source (BBS) that generates an optical spectrum from 1000nm to 2000nm. This broadband signal enters the demux filter centered at 1550nm. The pass bands of the filter sliced optical bandwidths of 1nm, 3nm, 6nm and 8nm that were used as optical sources to the Mach-Zehnder Modulator (MZM). The approach is evaluated in terms of the performance provided by using broadband optical slices and its impact on the available bandwidth modulation capability. Also, by measuring the Error Vector Magnitude (EVM), the quality of the transported signals was also assessed. For the experimental validation a Vector Network Analyzer (VNA) feeds the system with frequencies from 5MHz up to 5GHz. Then, the optical modulated signal is amplified 15 dB before the transmission through the optical fiber. After the propagation on fiber of the

SCM signals, an optical attenuator (ATT) emulates additional optical losses of the approach and a Photo Detector (PD) enables the analysis and evaluation of the transported signals.

The layout of the implementation for the experimental demonstration is shown in Fig. 2 and a simulation model was carried out in order to evaluate the performance of the approach under different parameter configurations in Optisystem, the results are described in section III.A. The experimental demonstration was performed with the arbitrary waveform generator M8190A where the I/Q signals where generated and subsequently up-converted in the E8663D PSG RF analog signal generator. The down-conversion was performed in the N9020A (MXA) Signal Analyzer. In this scenario, Dual-Polarization Quadrature Phase Shift Keying (QPSK) and the 16QAM (Quadrature Amplitude Modulation) transporting 10 Mbauds onto 3GHz were used.



Fig. 1. Layout of the centralized spectral slicing for access-metro networks. Source: Authors.



Fig. 2. Layout of the experimental demonstration for the proposed system. Source: Authors.

III. RESULTS

The results of the power characterization for the defined pass bands given by the slicing filter at different fiber lengths are shown in Fig. 3. As it can be seen, the thinner the slice size the lower the optical power and the wider the pass band the higher the power available per carrier. It means that the slice size impacts directly on the optical power available per generated carrier. For that reason an EDFA amplifier was used to increase the power level at the transmitter output in the experimental characterization.



Fig. 3. Power as a function of the slice size. Source: Authors.

Fig. 4 shows the behavior of different RF frequencies against different slice sizes at different lengths. As seen, shorter distances imply wider modulation bands e.g. in the case of a pass band of 1nm, a modulation band of 2.7 GHz was found for 1 km fiber length. In this scenario, it was generally observed that the modulation band capacity decreases as the pass band and transmission distance increases. It is also worth mentioning that no dispersion compensation process was performed, which implies that the results for the 5 and 10 km case can be improved in terms of the available modulation bandwidth of the generated carrier. In the same way, the carrier suppression effect was not observed in the experimental assessment. Fig. 5 depicts the constellations for 3GHz SCM/QPSK and 3GHz SCM/16QAM on 1nm, 3nm, 6nm and 8nm slice sizes respectively. It is observed that for a slice size of 1nm the constellation is clean in both modulations, whereas for a pass band of 3nm and 6nm respectively the constellations turn noisier particularly in the 16QAM modulation.



Fig. 4. Bandwidth modulation as a function of the slice size. Source: Authors.



Fig. 5. Experimental results: (a) Constellation for 3 GHz SCM/QPSK. (b) 3 GHz SCM/16QAM. Measurements performed after a 10 km optical link. Source: Authors.

For a pass band of 8 nm the signal is not detectable at all in any of the evaluated modulations. These facts demonstrate that the quality of the signal is reduced, as the slice sizes are broader. In this context, broader slice sizes affect the higher multilevel modulation significantly due to the accumulated chromatic dispersion, which prevent to get a tolerable quality of signal. Such behavior can be observed in Fig. 6 where the EVM per subcarrier and EVM per symbol were measured for the QPSK service transported onto a subcarrier of 3GHz. Fig. 6(a) shows the results for a 1nm optical slice size, Fig. 6(b) depicts the results for an slice size of 3nm and Fig. 6(c) shows the performance for a slice size of 6nm.



These results confirm that the EVM improves, as the slice size is narrower due to the relative lower impact of the chromatic dispersion as seen in the constellations shown in Fig. 5. Notice that for 1nm and 3 nm slice sizes the EVM is around 20% whereas for 6nm the EVM scales up to 40% in the QPSK modulation. Fig. 7 summarizes the behavior of the QPSK and 16 QAM modulation formats at 1 GHz and 3 GHz subcarriers transported on the defined pass bands and a constant fiber length of 10 km. For the case of 1nm pass band transporting 1GHz SCM/QPSK, the EVM was 29.6% while an EVM of 42.3% was measured for 1GHz SCM/16QAM. Note that the degradation depends on the available pass band and on the modulation used as observed in the constellations shown in Fig. 5. The results obtained with slice sizes broader than 6nm indicate that unless additional processing to mitigate the chromatic dispersion is included, this pass band is not suitable to transport a subcarrier-multiplexed service with a good level of quality assurance.



Fig. 7. Experimental results: EVM measurement for 1GHz SCM/QPSK, 1GHz SCM/16QAM, 3GHz SCM/QPSK and 3 GHz SCM/16QAM. Source: Authors.

A. Simulation results

The simulation based modeling of the general scheme was performed in Optisystem in order to assess the approach based on the subcarrier frequency, the distance and the pass band parameters. Unlike the experimental assessment, the carrier suppression effect indeed appeared in the simulations due to the longer distances evaluated. It must be also pointed out that the modeling evaluation includes narrower slice sizes and different services as compared to those used in the experimental assessment described previously. This fact allows evaluating the performance using different types of filters and pattern traffic transported in the system. In this context, the modeled slice sizes were 100MHz and 200 MHz and the bit rate was 1Gb/s Non-Return to Zero (NRZ) encoded that was assessed through the Q factor measurement. As far the subcarrier is concerned, 5GHz, 30GHz and 60GHz were used. The transmission distance was swept from 5km

Fig. 6. Experimental results: EVM per subcarrier and EVM per symbol for the QPSK service at 3GHz transmitted at different optical bandwidths, (a) 1nm. (b) 3nm. (c) 6nm. Source: Authors.

to 50km in steps of 5km, Fig. 8 and Fig. 9 show the corresponding results for an optical pass band of 100MHz and 200 MHz respectively. The results obtained in the conducted simulations for a 100MHz optical pass band used, show that by considering a limit Q factor of 7 (dotted line in Fig. 8), which roughly corresponds to a bit error rate of 1x10⁻¹², the subcarriers at 5GHz and 30GHz reach a propagation distance of up to 50km while the 60GHz subcarrier reaches the quality of signal limit at a maximum propagation of 40km.

Notice in Fig. 9 the strong degradation of the Q factor when a slice size of 200MHz was used as compared to the result found for a slice size of 100MHz. This fact is due to the pulse broadening effect caused by a broader optical carrier. In this case only the 30GHz subcarrier is able to satisfy the quality of signal limit only at certain transmission distances. This interesting behavior comes from two reasons; the first one is due to the strongly number of harmonic distortion products that are absorbed by the photodetector with a 5GHz subcarrier, whereas the degradation of the 60GHz comes from the bandwidth limitation of the optical modulator used in the simulations. The second reason for such behavior is due to the higher differential group delay generated by the 200MHz optical pass band, which in turn causes the generation of the carrier suppression effect that makes the signal at 30GHz unable to be recovered from 9km to 21km and from 28km to 37km.



IV. CONCLUSIONS

This paper evaluates the use of a broadband light source and a wideband optical filter in order to generate optical carriers for the transmission of subcarrier-multiplexed signals in next generation access networks. The approach was evaluated through experimental demonstration and simulation modeling. Based on the conducted experimental measurements, the power response of the system improves depending on the optical pass band defined in the slicing filter at subcarrier frequencies below 1 GHz. It was observed that the narrower the pass bands in the filter, the better the response in the receiver due to the chromatic dispersion penalties imposed by the standard monomodo optical fiber. However, it should be taken into account that a narrow optical pass band leads to a lower average optical power. Thus, the signal quality depends on the compromise between the optical power and the dispersion for a given optical pass band. The experimental results demonstrated that the 16QAM modulation is recommended only when the subcarrier frequency is 1GHz or below, the optical pass band is lower than 3nm and the maximum length link is 10km in order to enable a correct equalization of the received signal. The measured EVM did not show significant difference regarding the subcarrier frequency for a QPSK service; therefore, a QPSK format modulated onto an optical subcarrier is feasible to be transported within broadband optical carriers up to 6nm wide over a fiber link of 10km. The modeling results allowed predicting the performance of the proposed approach at higher subcarrier frequencies and longer optical links using narrow slice sizes. Thus, a 60GHz subcarrier-multiplexed system over 40km and a slice size of 100MHz is suitable to satisfy 1x10⁻¹²-bit error rate. 5GHz and 30GHz subcarrier frequencies reach up to 50km due to the reduced contribution of the chromatic dispersion. For a slice size of 200MHz the combination of the accumulated differential group delay, distance and subcarrier frequency causes the carrier suppression effect which prevents a proper operation of the system. This effect could not be observed in the experimental demonstration due to the shorter distance evaluated a lower value of the subcarrier frequency used. Overall, the results found in the experimental measurements and the simulation modeling demonstrate the feasibility of the proposed approach to generate a multicarrier optical signal for subcarrier multiplexed networks that provide the transport to future mobile systems.



Fig. 9. Modeling results: Q factor vs. distance for 200MHz pass band. Source: Authors.

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