

## REGULAR ARTICLE

## Physics &amp; Engineering

# Stability Performance of a Quantum Square-shaped Extended Source P-N-P-N TFET with Silicon Carbide Substrate by Means of a Physics-Based Analytical Model

Desempeño de Estabilidad de una Fuente Cuántica Cuadrada Extendida P-N-P-N TFET con Sustrato de Carburo de Silicio Mediante un Modelo Analítico Físico

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## 1 | INTRODUCTION

Tunneling field-effect transistors (TFETs) based on band-to-band tunneling (BTBT) mechanism are considered to be a promising solution to the downscaling and power crisis of the complementary metal oxide semiconductor (CMOS) in low standby power (LSTP) devices. In particular, TFETs can achieve sub-60 mV/decade

**ABSTRACT.** In this paper, an analytical stability model for quantum square-shaped extended source P-N-P-N tunneling field-effect transistor (P-N-P-N TFET) with silicon carbide substrate is developed that includes the effects of gate-source capacitance, gate-drain capacitance, effective gate resistance, time constant and transconductance. A nonquasistatic RF small-signal model has been used and stability that was extracted from analytical equations of its Y-parameters. The obtained analytical expression for stability is compared with device simulation results and excellent agreement is found up to 100 GHz. The stability performance of a quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate is also studied analytically considering pocket width and doping variation. The results strongly confirm that the proposed model is accurate and suitable for the quantum square-shaped extended source P-N-P-N TFET in the high-frequency regime.

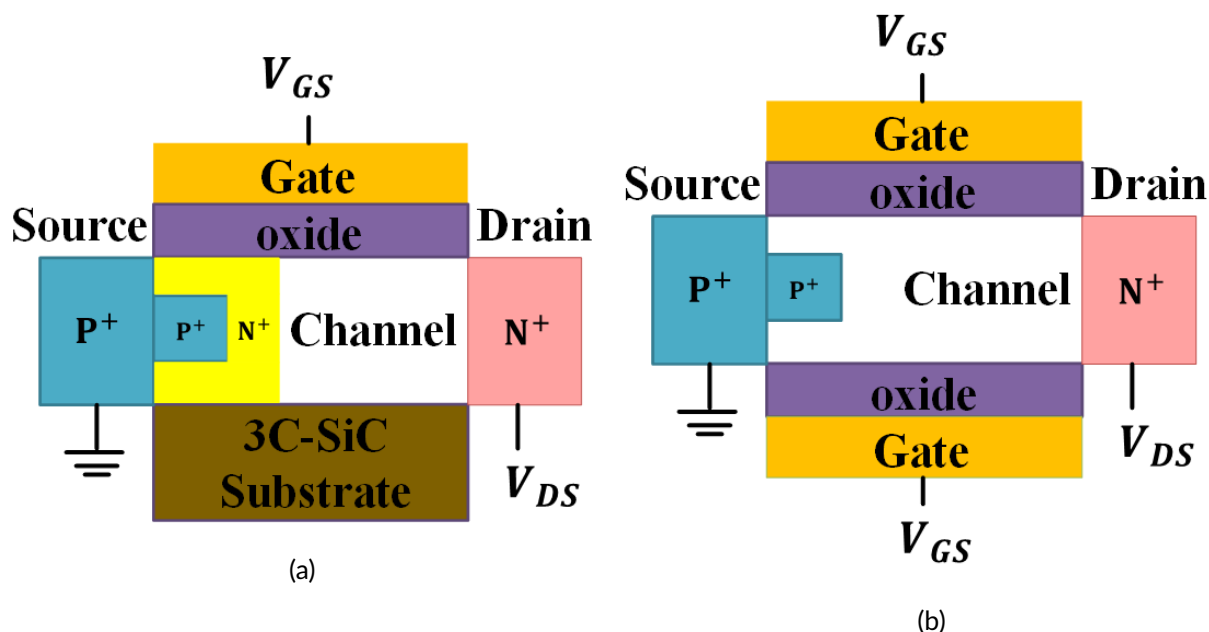
**keywords:** Analytical modeling; Nonquasistatic (NQS); Quantum extended source, stability; silicon carbide; P-N-P-N Tunneling field-effect transistor (P-N-P-N TFET).

**RESUMEN.** En este documento, se desarrolla un modelo de estabilidad analítica para el transistor de efecto de campo de túnel PNP de fuente extendida cuántica de forma cuadrada (PNPN TFET) con sustrato de carburo de silicio que incluye los efectos de la capacitancia de fuente de compuerta, capacitancia de drenaje de compuerta, resistencia efectiva de compuerta, constante de tiempo y transconductancia. Se ha utilizado un modelo de señal pequeña RF no cuantitativo y una estabilidad que se extrajo de las ecuaciones analíticas de sus parámetros Y. La expresión analítica obtenida para la estabilidad se compara con los resultados de la simulación del dispositivo y se encuentra que los resultados coinciden bien hasta 100 GHz. El rendimiento de estabilidad de un TFET P-N-P-N de fuente extendida cuántica con sustrato de carburo de silicio también se estudia analíticamente considerando el Pocket-Width y la variación de dopaje. Los resultados confirman que el modelo propuesto es preciso y adecuado para la fuente extendida cuántica de forma cuadrada P-N-P-N TFET en el régimen de alta frecuencia.

**Palabras clave:** Modelos analíticos; No cuasi-estático (NQS); Fuente cuántica extendida, Estabilidad; Carburo de silicio; P-N-P-N Transistor de efecto de campo de túnel (TFET P-N-P-N).

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subthreshold slope (SS) at room temperature, enabling ultralow power dissipation and suppressed short channel effects (SCE) [1, 2, 3]. A lot of research has been done in the area of TFETs in terms of the design, modeling, fabrication, and characterization [4]-[28]. The stability is one of the important parameters in the selection of transistor to design the radio-frequency (RF) amplifier and integrated circuit. Generally, there are two possible types for devices stability. One is the unconditionally stable device that is preferred for the RF design because its stability is port impedance-independent. The other is potentially stable device that causes significant performance degradation and the noise level increase, due to need of additional stabilization network. Marjani et al. presented the RF small-signal model for square-shaped extended source tunneling field-effect transistor in the context of careful consideration of gate-source capacitance, gate-drain capacitance, effective gate resistance, time constant and transconductance using a combination of nonquasistatic RF small-signal modeling, device simulations, and SPICE verification [20].



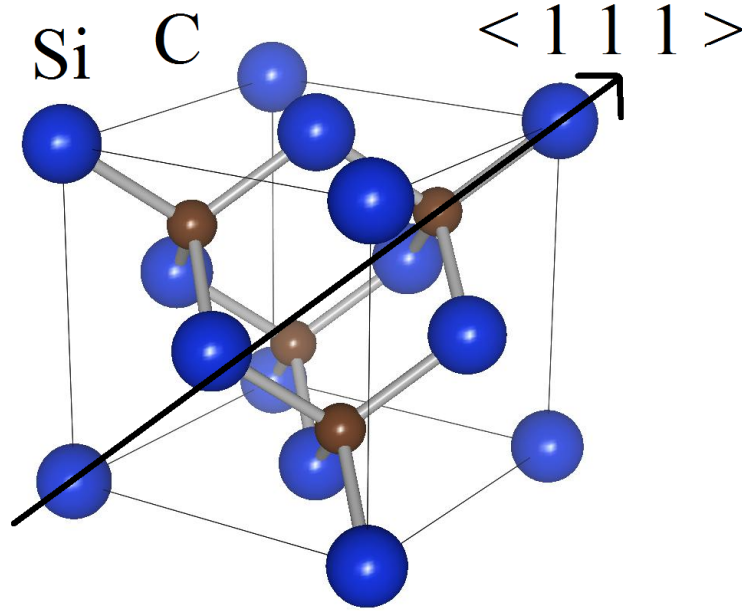
**FIG. 1** Cross-sectional views of the (a) quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate, (b) conventional square-shaped extended source TFET structures.

In this paper, an analytical stability model for quantum square-shaped extended source P-N-P-N tunneling field-effect transistor (P-N-P-N TFET) with silicon carbide substrate is developed that includes the effects of gate-source capacitance, gate-drain capacitance, channel resistance, time constant and transconductance. The stability was extracted from analytical equations of  $Y$ -parameters that were evaluated by two-dimensional device simulator simulation using stimulating multiple models including nonlocal band-to-band tunneling model, auger recombination, trap assisted tunneling model, band-gap narrowing, Shockley-Read-Hall recombination model, Hurkx recombination model, concentration dependent mobility model and field dependent mobility model. The paper is organized as follows: Section 2 describes the device structures and model formulation of stability for quantum square-shaped extended source P-N-P-N TFET. Section 3 presents the model validation, results and discussion. In Section 4, we conclude.

## 2 | DEVICE STRUCTURE AND MODEL FORMULATION OF STABILITY FOR QUANTUM SQUARE-SHAPED EXTENDED SOURCE P-N-P-N TFET

Fig. 1 (a) and (b) show cross-sectional views of the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate and conventional square-shaped extended source TFET devices for simulations

in Silvaco ATLAS software [29]. The heavily doped pocket and square-shaped extended source regions can be achieved by a tilt angled implant before the gate stack formation and high-energy and low-current boron implantation after the pocket formation [6][20]. The 3C-SiC is one of silicon carbide polytypes that have been concerned as the today's semiconductor materials. It has the high electron mobility and saturation velocity because of the reduced scattering [30] that its lattice structures is shown in Fig. 2.



**FIG. 2** The crystal structure of cubic silicon carbide polytype (3C-SiC).

The simulated devices are the channel doping concentrations  $10^{15} \text{ cm}^{-3}$ , source doping concentrations  $10^{20} \text{ cm}^{-3}$ , drain doping concentrations  $10^{20} \text{ cm}^{-3}$ , pocket doping concentrations  $10^{19} \text{ cm}^{-3}$ , body thickness of  $15 \text{ nm}$ ,  $2 \text{ nm}$  gate oxide thickness and  $30 \text{ nm}$  of gate length.

The  $Y$ -parameters of the nonquasistatic RF small-signal model for square-shaped extended source tunneling field-effect transistor in the context of careful consideration of gate-source capacitance ( $C_{gs}$ ), gate-drain capacitance ( $C_{gd}$ ), effective gate resistance ( $R_g$ ), time constant ( $\tau$ ) and transconductance ( $g_m$ ) can be expressed as [20]:

$$Y_{11} = \frac{\omega^2 R_g (C_{gs} + C_{gd})^2 + j\omega (C_{gs} + C_{gd})}{1 + \omega^2 R_g^2 (C_{gs} + C_{gd})^2}, \quad (1)$$

$$Y_{12} = \frac{-\omega^2 R_g C_{gd} (C_{gs} + C_{gd}) - j\omega C_{gd}}{1 + \omega^2 R_g^2 (C_{gs} + C_{gd})^2}, \quad (2)$$

$$Y_{21} = \frac{-j\omega C_{gd} - \omega^2 R_g C_{gd} (C_{gs} + C_{gd})}{1 + \omega^2 R_g^2 (C_{gs} + C_{gd})^2} + \frac{g_m - j\omega g_m [\tau + R_g (C_{gs} + C_{gd})] - \omega^2 R_g g_m \tau (C_{gs} + C_{gd})}{[1 + \omega^2 R_g^2 (C_{gs} + C_{gd})^2] (1 + \omega^2 \tau^2)}, \quad (3)$$

and

$$Y_{22} = \frac{-j\omega C_{gd} - \omega^2 R_g C_{gd} (C_{gs} + C_{gd})}{1 + \omega^2 R_g^2 (C_{gs} + C_{gd})^2} + \frac{g_m - j\omega g_m [\tau + R_g (C_{gs} + C_{gd})] - \omega^2 R_g g_m \tau (C_{gs} + C_{gd})}{[1 + \omega^2 R_g^2 (C_{gs} + C_{gd})^2] (1 + \omega^2 \tau^2)} \quad (4)$$

where  $\{Y_{mn}\}$  with  $m = 1, 2$  and  $n = 1, 2$  are complex parameters and  $j = \sqrt{-1}$  is the imaginary unit. By using real and imaginary parts of Eqs. 1-4 and considering some assumptions, The analytical values of device small signal parameters can be obtained as [20]:

$$g_m = \operatorname{Re}[Y_{21}]|_{\omega^2=0}, \quad (5)$$

$$g_{ds} = \operatorname{Re}[Y_{22}]|_{\omega^2=0}, \quad (6)$$

$$R_g = \frac{1}{(\operatorname{Im}[Y_{11}])^2} \operatorname{Re}[Y_{11}], \quad (7)$$

$$C_{gs} = \frac{1}{\omega} (\operatorname{Im}[Y_{11}] + \operatorname{Im}[Y_{12}]), \quad (8)$$

$$C_{gd} = -\frac{1}{\omega} \operatorname{Im}[Y_{12}], \quad (9)$$

$$\tau = -\frac{1}{g_m} \left[ \frac{\operatorname{Im}[Y_{12}]}{\omega} + C_{dg} + g_m R_g (C_{gs} + C_{gd}) \right], \quad (10)$$

and

$$C_{ds} = \frac{1}{\omega} \operatorname{Im}[Y_{22}] - C_{gd} - R_g g_m C_{gd}. \quad (11)$$

The stability of TFET can be expressed at different frequencies of operation in terms of Y-parameters as follows [31]:

$$k = \frac{2\operatorname{Re}[Y_{11}]\operatorname{Re}[Y_{22}] - \operatorname{Re}[Y_{12}Y_{21}]}{|Y_{12}Y_{21}|} \quad (12)$$

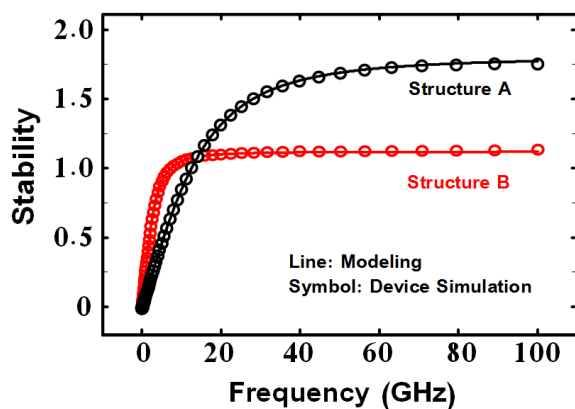
In order to simplify further, by substituting the  $Y$ -parameters into (12), the analytical equations for stability are obtained as a function of the small-signal parameters as below:

$$k = \frac{\omega^2 \{ (C_{gd}^2 + 2(C_{gs} + C_{gd})[C_{gs}g_{ds} + C_{gd}(g_{ds} + g_m)]R_g + C_{gd}g_m\tau) \}}{\sqrt{g_m^2 + (C_{gd} + g_m\tau)^2\omega^2(C_{gd}\omega + C_{gd}(C_{gs} + C_{gd})^2R_g^2\omega^3)}} + \frac{\omega^4 \{ C_{gd}(C_{gs} + C_{gd})^2R_g^2(C_{gd} + 2C_{gd}g_mR_g + g_m(2C_{gs}R_g + \tau)) \}}{\sqrt{g_m^2 + (C_{gd} + g_m\tau)^2\omega^2(C_{gd}\omega + C_{gd}(C_{gs} + C_{gd})^2R_g^2\omega^3)}} \quad (13)$$

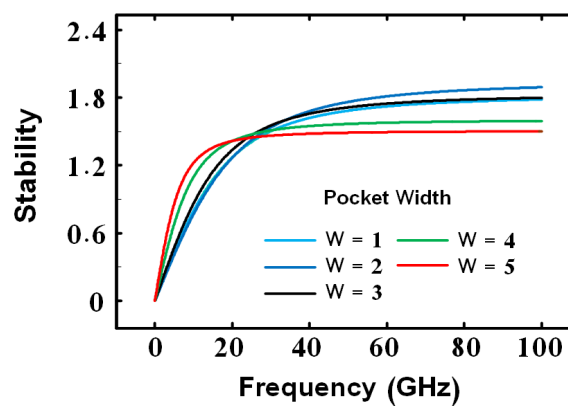
### 3 | MODEL VALIDATION, RESULTS AND DISCUSSION

To verify the validity of the proposed model, stability of the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate and conventional square-shaped extended source TFET devices are

simulated using the Silvaco ATLAS device simulator [29]. Fig. 3 compares the stability that were obtained from the analytical model and the simulated values as a function of the frequency for the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate (Structure A) and conventional square-shaped extended source TFET (Structure B) with  $30nm$  gate length in the on-state ( $V_g = 1.5V$  and  $V_d = 1V$ ). As seen, an excellent agreement for the stability of analytical model and device simulation is achieved up to the  $100GHz$  regime. In addition, the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate has higher shows a better stability compared to conventional square-shaped extended source TFET because of its higher transconductance and gate-drain capacitance. Without any optimization, the root mean square (RMS) error of the model was calculated to be within 1.25% up to  $100GHz$ . These verification results strongly support that the model is accurate and valid for quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate and conventional square-shaped extended source TFET up to the extremely high frequency range.



**FIG. 3** Comparison of modeling and device simulation values of stability for quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate (Structure A) and conventional square-shaped extended source TFET (Structure B) structures.

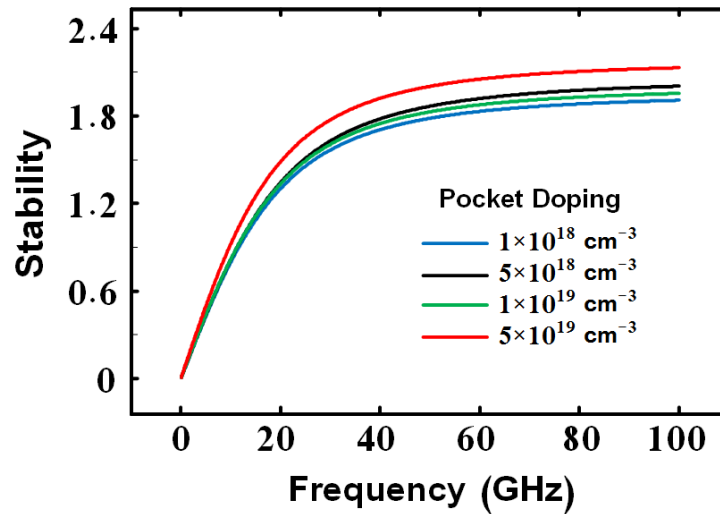


**FIG. 4** Variation of stability of quantum square-shaped extended source P-N-P-N TFET versus frequency for various values of pocket width.

In addition, we analyze analytically the dependence of the stability on pocket parameters including width and doping variation. Fig. 4 shows the impact of varying width of pocket ( $W$ ) with constant doping concentration of  $1 \times 10^{-19} cm^{-3}$  on the stability of a quantum square-shaped extended source P-N-P-N TFET biased at  $V_D = 1V$ . Five different values of pocket width 1, 2, 3, 4 and  $5nm$ , are used for this purpose. On one hand, on-current and transconductance of device increases as pocket width increases. This is mainly because the well region containing the local minimum of the conduction energy band edge becomes wider, which increases the probability of the tunneling of electrons from source to drain, and thus on-current increases. But on the other hand, an increasing pocket width results in increasing gate-drain capacitance. Especially for very wide pocket width, pocket begins to be partially depleted and declines the on-current and transconductance. Since pocket width of 2 produces the best performance of the stability, it is used for the rest of this paper. Also, the critical frequency values of above-mentioned devices with 1, 2, 3, 4 and  $5nm$  pocket width are about 13.3, 13.5, 11.7, 8.3 and  $6.7GHz$ , respectively. This indicates that the quantum square-shaped extended source P-N-P-N TFET does not require the additional stability circuits for RF circuits above these frequencies. This model fits well with RMS error within 1.13% up to  $100GHz$ .

Fig. 5 shows the stability for four different values of pocket doping concentration ( $N_p$ ) as  $1 \times 10^{18}$ ,  $5 \times 10^{18}$ ,  $1 \times 10^{19}$ , and  $5 \times 10^{19} cm^{-3}$  with constant width of  $2nm$ . As seen, the use of relatively high pocket doping concentration results in the enhancement of stability. This is mainly because of the high on-current and transconductance induced by the narrower tunneling barrier width at the source-channel interface. It is also observed that the pocket doping concentration plays an important role in determining the critical frequency. The value

of critical frequency reaches 13 GHz for lower pocket doping concentration ( $N_p = 1 \times 10^{18} \text{ cm}^{-3}$ ) as compared to higher pocket doping concentration ( $N_p = 5 \times 10^{19} \text{ cm}^{-3}$ ) with critical frequency greater than 10GHz. The RMS error between modeled and simulated values for four different values of pocket doping concentration is only 1.65% . The results of model verification confirm that the model is highly reliable and available for the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate.



**FIG. 5** Variation of stability of quantum square-shaped extended source P-N-P-N TFET versus frequency for various values of pocket doping concentration.

#### 4 | CONCLUSION

In this paper, we develop an analytical stability model for quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate by considering the effects of gate-source capacitance, gate-drain capacitance, effective gate resistance, time constant and transconductance. The analytical expression of stability is obtained from Y-parameters equations of a nonquasistatic RF small-signal model. The stability performance of a quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate is compared with the conventional square-shaped extended source TFET and excellent agreement is found up to 100 GHz. In addition, the width and doping dependence of pocket on performance of the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate has been studied. The results indicate that the proposed model is accurate and suitable for the quantum square-shaped extended source P-N-P-N TFET with silicon carbide substrate in the high-frequency regime up to 100 GHz.

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